Effect of Elastic Moduli Mismatch on Particulate Fracture in AA7020/Silicon Nitride Particulate Metal Matrix Composites

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Abstract: Hexagonal array unit cell/spherical particulate RVE models were employed to predict particulate fracture using two-dimensional finite element methods under plane strain conditions. The particulate metal matrix composites are silicon nitride/AA7020 alloy at different volume fractions of silicon nitride. There is strong probability of silicon nitride particulate fracture at its high (30%) volume fraction in the AA7020 alloy matrix.

Keywords: AA7020, silicon nitride, round particle, RVE model, finite element analysis, particulate fracture.

1. INTRODUCTION

The property of metal matrix composites was improved by the uniform distribution of reinforcement and the refinement of subgrain size particulates. Since most ceramics are available as particles, there is a wide range of potential reinforcements for particle reinforced composites [104-108]. The particulate materials are silicon carbide [1], boron carbide [2-4], alumina [5] and titanium boride [6-8]. Silicon nitride particulates were tested with matrix alloys such as AA1100 alloy [9], AA2024 alloy [10], AA3003 alloy [11] and AA4015 alloy [12]. The AA 7020 alloy is a high strength material used for highly loaded structural applications.

The aim of the present paper is to predict the particle fracture of AA7020 alloy/silicon nitride particulate metal matrix composites. Finite element method is used to construct and analyze representative volume elements (RVEs) models of periodic circular particulates in a hexagonal array distribution.



Figure 1: The RVE model: (a) particle distribution and (b) RVE scheme.

2. MATERIALS AND METHODS

The AA7020 alloy/ silicon nanoparticulate metal matrix composites were used in the present work with 10%, 20%, and 30% volume fractions of silicon nitride. The periodic model for the representative volume element (RVE) scheme as shown in fig-

(3)

(4)

ure 1 was used to analyze the composites with finite element software code. The RVE scheme was abstracted from round particulates in hexagonal array particulate distribution. The perfect adhesion was assumed between silicon nitride particle and AA7020 alloy matrix. PLANE183 element was used for the matrix and the nanoparticle. The interface between particle and matrix was modeled using CONTACT -172 elements.

If particle fracture occurs when the stress in the particle reaches its ultimate tensile strength, $\sigma_{p,uts}$, then setting the boundary condition at

$$\sigma_{p} - \sigma_{p, uts}$$
 (1)
and substituting into Eq.(1) gives a relationship between the strength of the particle and the interfacial shear stress such that if
 $\sigma_{P,uts} < \frac{2\tau}{n}$ (2)

Then the particle will fracture. Similarly if interfacial debonding/yielding is considered to occur when the interfacial shear stress reaches its shear strength

$$\tau = \tau_{max}$$

Then by substituting Eq. (5) into Eq.(1) a boundary condition for particle/matrix interfacial fracture can be established whereby,

$$\tau_{\rm max} < \frac{n\sigma_p}{2}$$

This approach suggests that the outcome of a matrix crack impinging on an embedded particle depends on the balance between the particle strength and the shear strength of the interface.

3. RESULTS AND DISCUSSION

Influence of silicon nitride on the elastic moduli, E_x , E_y and Gxy are shown figure 2a. The tensile elastic modulus and shear modulus were nearly constant. The compressive elastic modulus was low for 30% silicon nitride in the matrix Aa7020 alloy. The major Poisson's ratio increases with increase of volume fraction of silicon nitride (figure 2b).



Figure 2: Effect of volume fraction on effective material properties.

The particulate fracture was observed at 30% silicon nitride in the composite as per the condition $\sigma_p \le 2\tau/n$ as shown in figure 3a. The debonding was also in all the composites as shown in figure 3b. The debonding and particulate was due to heavy load transfer the AA7020 matrix alloy to the silicon nitride particulates.

The stress induced in the particle or at the interface was higher than that induced in the matrix as shown in figure 4. The induced stresses increased with the increase of volume fraction of silicon nitride in the composites. The shear stress developed at the interface was approximately the same in all the composites (figure 4c). The interface debonding had occurred in the direction of tensile loading. The main reason for the particulate fracture was on account of the elastic moduli mismatch between the AA7020 alloy matrix and silicon nitride particulates. The elastic moduli of AA7020 alloy matrix and silicon nitride are, respectively, 72GPa and 317 GPa. The mismatch is 245 GPa.



Figure 3: Fracture criteria of: (a) particulate and (b) interface.



4. CONCLUSION

The interface debonding and silicon nitride particulate fractures took place at volume fraction of 30% SiN in the composite. The debonding was in the direction of the tensile loading. The elastic moduli mismatch between AA7020 alloy and silicon nitride is about 245 GPa.

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