

# Effect of Cold Rolling on Porosity and Micromechanical Properties of AA6061/Zirconium Carbide Metal Matrix Composites

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**Abstract:** The AA6061/ZrC alloy metal matrix composites were fabricated using stir casting process and analyzed for tensile properties in the presence of porosity. Porosity was measured with different volume percents of zirconium carbide particle reinforced to AA6061 alloy. The density increased with increase of ZrC particles in AA6061 alloy matrix. Development of porosity and increased content of reinforcement particles reduced the plastic deformation of matrix.

**Keywords:** Titanium oxide, AA6061 alloy, unit cell models, finite element analysis, porosity.

## 1. INTRODUCTION

Metal matrix composites have gained a considerable interest in the recent years because of the fact that addition of ceramic reinforcement in the metal matrix can improve specific strength, stiffness, wear, fatigue and creep properties compared to conventional engineering materials. Stir casting is one of the methods accepted for the production of large quantity commercially practiced [1-19]. It is attractive because of simplicity, flexibility and most economical for large sized components to be fabricated. It is a liquid state method of composite materials fabrication, in which a dispersed phase (ceramic particles, short fibers) is mixed with a molten matrix metal by means of mechanical stirring. The main factors that control the properties of metal matrix composites fabricated using casting techniques include: reinforcement distribution, wetting of reinforcement by matrix alloy porosity in the cast metal matrix and chemical reaction between reinforcement material and the matrix alloy [20-38].

The objective of this research work was to fabricate AA6061 alloy/zirconium carbide metal matrix composites using stir casting technique. The effects of porosity on micromechanical properties were investigated using experimental practice and finite element analysis. For the finite element analysis, the spherical shaped zirconium carbide particles were assumed to analyze unit cells with and without porosity.

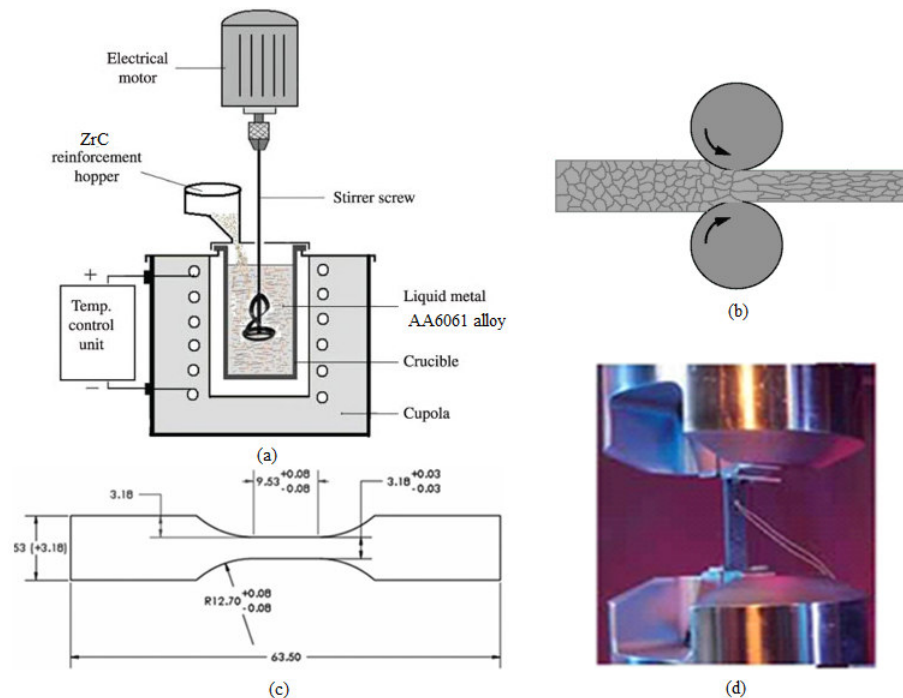


Figure 1: Stir casting process; cold rolling (b); shape and dimensions of tensile specimen (c); and tensile testing on UTM (d).

## 2. MATERIALS METHODS

The matrix material was AA6061 alloy. The reinforcement material was ZrC nanoparticles of average size 100nm. AA6061/ZrC alloy composites were fabricated by the stir casting process and low pressure casting technique with argon gas at 3.0 bar. The composite samples were give solution treatment and cold rolled to the predefined size of tensile specimens. The heat-treated samples were machined to get flat-rectangular specimens (figure 1) for the tensile tests. The tensile specimens were placed in the grips of a Universal Test Machine (UTM) at a specified grip separation and pulled until failure. The test speed was 2 mm/min. A strain gauge was used to determine elongation. In the current work, a unit cell comprising of nine particles was implemented to analyze the tensile behavior AA6061/ZrC composites at three (10%, 20% and 30%) volume fractions of ZrC. The large strain PLANE183 element was used in the matrix in all the models. In order to model the adhesion between the matrix and the particle, a CONTACT 172 element was used with reference to application of finite element method for several metal matrix composites. The finite element analysis was carried out on a unit cell without porosity as shown in figure 2a and that with porosity as shown in figure 2b.

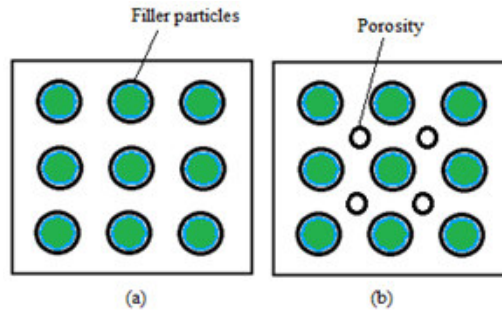


Figure 2: Unit cells: (a) without porosity and (b) with porosity.

Density of the composite is calculated from 'Rule of Mixture' as follows:

$$\left(\frac{v_p}{\rho_p} + \frac{1-v_p}{\rho_m}\right) \leq \rho_c \leq (1 - v_p)\rho_m \quad (1)$$

where  $v_p$  is the volume fraction of particles and  $\rho_c$ ,  $\rho_p$ , and  $\rho_m$  are densities of composite, particles and matrix, respectively.

Considering adhesion, formation of precipitates, particle size, agglomeration, voids/porosity, obstacles to the dislocation, and the interfacial reaction of the particle/matrix, the formula for the strength of composite is stated below:

$$\sigma_c = \left[ \sigma_m \left\{ \frac{1-(v_p-v_v)^{2/3}}{1-1.5(v_p-v_v)} \right\} \right] e^{m_p(v_p-v_v)} + k d_p^{-1/2} \quad (2)$$

$$k = E_m m_m / E_p m_p$$

where,  $v_v$  and  $v_p$  are the volume fractions of voids/porosity and nanoparticles in the composite respectively,  $m_p$  and  $m_m$  are the poisson's ratios of the nanoparticles and matrix respectively,  $d_p$  is the mean nanoparticle size (diameter) and  $E_m$  and  $E_p$  is elastic moduli of the matrix and the particle respectively. Elastic modulus (Young's modulus) is a measure of the stiffness of a material and is a quantity used to characterize materials. Elastic modulus is the same in all orientations for isotropic materials. Anisotropy can be seen in many composites.

The upper-bound equation is given by

$$\frac{E_c}{E_m} = \left( \frac{1-v_v^{2/3}}{1-v_v^{2/3}+v_v} \right) + \frac{1+(\delta-1)v_p^{2/3}}{1+(\delta-1)(v_p^{2/3}-v_p)} \quad (3)$$

The lower-bound equation is given by

$$\frac{E_c}{E_m} = 1 + \frac{v_p-v_v}{\delta/(\delta-1)-(v_p+v_v)^{1/3}} \quad (4)$$

where,  $\delta = E_p/E_m$ .

## 3. RESULTS AND DISCUSSION

The tensile strength was increased due to addition of ZrC particles without porosity AA6061/ ZrC metal matrix composites; it decreased with porosity (figure 3a). The tensile stresses obtained from the finite element analysis (FEA) were higher than those obtained from the mathematical expression mentioned in Eq.(2) and the experimental procedure as shown in figure 3a. The density increased with increase of volume fraction of ZrC in the AA6061 alloy matrix (figure 3b). The reason could be attri-

butted increasing volume percentages of reinforced particles were added to the base matrix. The densities of ZrC and AA6061 alloy are, respectively, 6.73 g/cc and 2.70 g/cc. The porosity presence has affected the yield strength, ductility, Poisson's ratio and ultimate tensile strength of metal matrix composites [38, 39]. This is confirmed with the microstructures of the composites shown in figure 4.

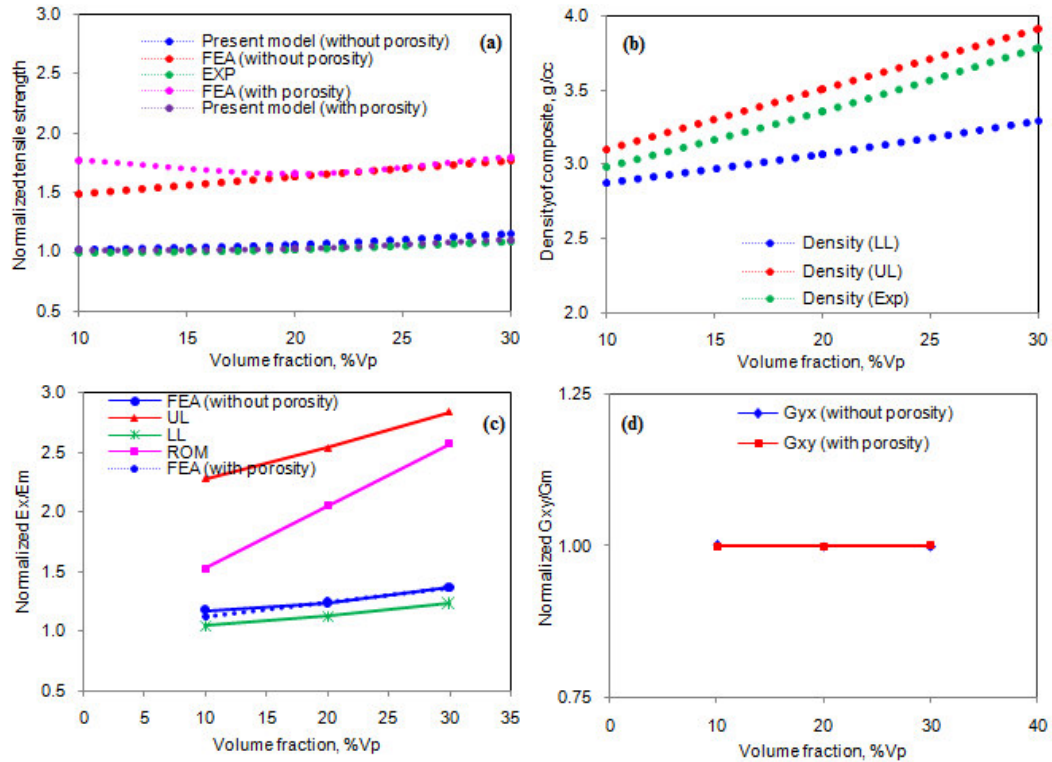


Figure 3: Effect of volume fraction on (a) normalized strength, (b) normalized tensile elastic modulus, (c) normalized shear modulus and (d) density of AA6061/ ZrC composites.

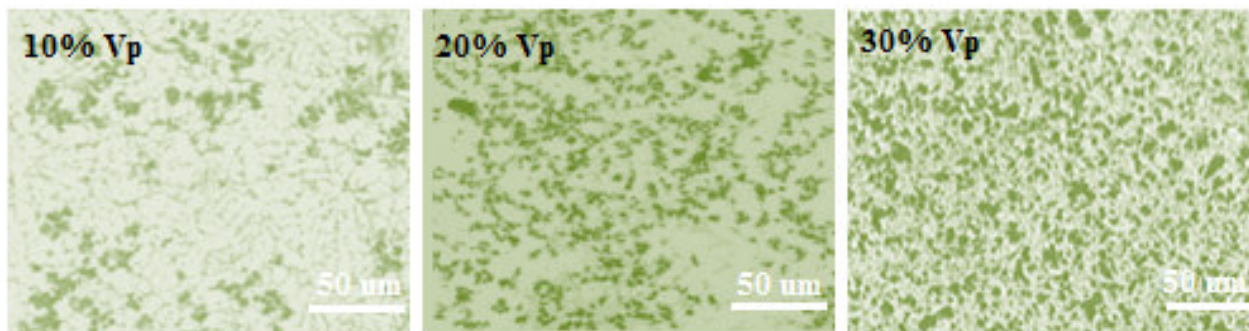


Figure 4: Microstructure showing porosity and distribution of 10%, 20% and 30% ZrC nanoparticles in AA6061 alloy matrix.

The normalized elastic modulus increased with increase of volume fraction of ZrC particles in AA6061 alloy matrix with or without porosity. This is due to the increase of tensile beyond allowable tensile stress and decrease of ductility simultaneously. The normalized shear modulus was constant with increase of volume fraction of ZrC in the AA6061 alloy matrix with or without porosity (figure 3d). Without porosity in the composites, the tensile stress increased with increase of volume fraction of ZrC in AA6061 alloy matrix. The tensile stress was exceeded the allowable stress in the composites with porosity for the same load as that applied on the composites without porosity as shown in figure 5b. This is attributed to the development of the stress concentrations in the vicinity of the porosity especially in the composites having 30%ZrC particles. Development of porosity and increased content of reinforcement particles reduced the plastic deformation of matrix at which point failure initiated.

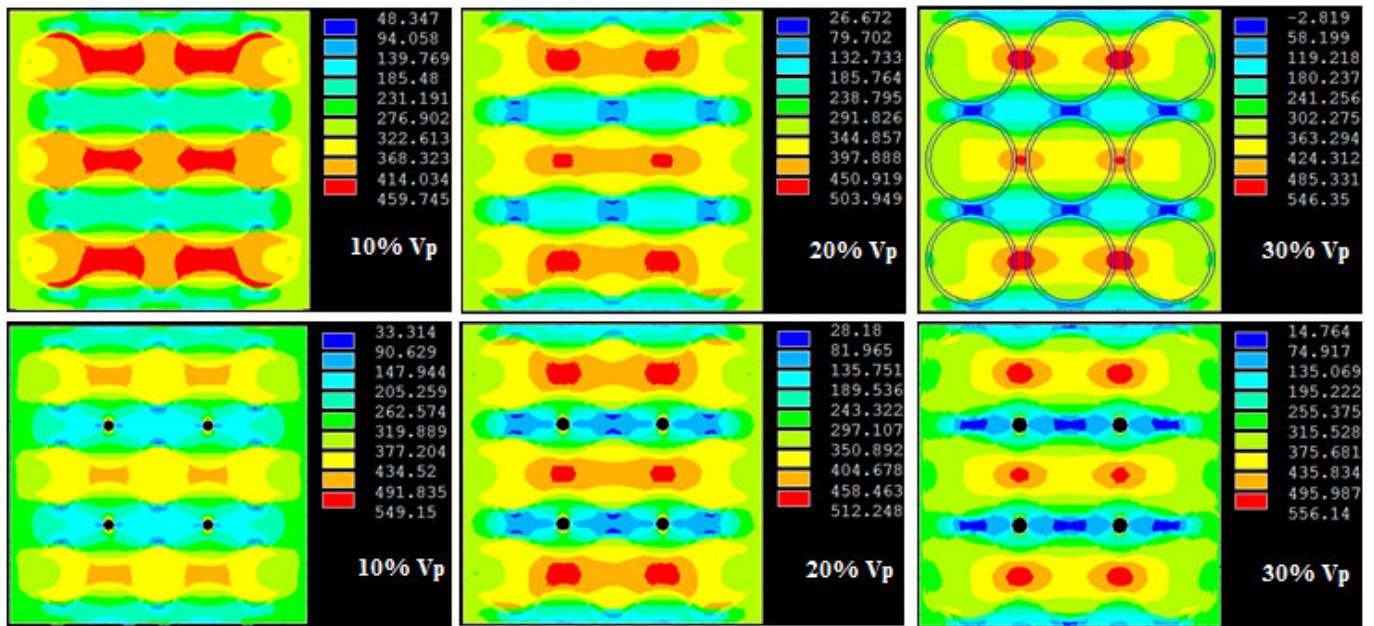


Figure 5: Images of tensile stresses obtained from FEA: (a) without porosity and (b) with porosity.

#### 4. CONCLUSIONS

Porosity content was significantly linear with increasing percentage of ZrC particles in AA6061 alloy matrix. In the presence of voids, the tensile stresses developed in the composites have exceeded the allowable stress for the same load applied on all the composite specimens reducing the plastic deformation of matrix.

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